## **AMENDMENTS TO THE CLAIMS:**

This listing of claims will replace all prior versions, and listings, of claims in the application:

## **Listing of Claims:**

Claim 1 (currently amended): Method for the production of a threedimensionally shaped structural part having a basic metal sheet and at least one smaller locally arranged reinforcing metal sheet, comprising connecting the basic metal sheet, in a flat state or in an incompletely formed preforming state, to the reinforcing metal sheet at a point predetermined for a subsequent reinforcing point, and subsequently joint forming the parts of a resulting patched composite metal sheet structure by an openable and closeable forming tool in a forming press, wherein heating of the patched composite metal sheet structure before the joint forming to a temperature which is above a forming temperature of the material, then forming the patched composite metal sheet structure in a hot state into a desired shape with subsequently cooling thereof in the forming tool in a closed state, or in a following fixing tool, with a desired forming state being fixed mechanically, and parts of the patched composite sheet metal structure are heated to above a structural transformation temperature of the material above which the material structure is in an austenitic state.

Claim 2 (canceled).

Claim 3 (original): Method according to Claim 1, wherein the patched

composite sheet structure is heated before joint forming to a specific

temperature within a temperature range between 850°C and 930°C.

Claim 4 (original): Method according to Claim 1, wherein the at least

one reinforcing sheet or at least one of the reinforcing sheets is itself preformed,

before being combined with the basic sheet, by affixation of reinforcing beads, in

such a way that said reinforcing sheet nevertheless can come to bear in a

dimensionally accurate manner at the predetermined point on the basic sheet

and can be fixed to the latter.

Claim 5 (currently amended): Method according to Claim 1, wherein

extraction of the heated composite sheet structure from a heating furnace, and

introduction of the composite sheet structure in a defined position into the open

forming tool up to the commencement of closing of the forming tool take place in

a timespan of less than three seconds, preferably less than two seconds.

Claim 6 (original): Method according to Claim 1, wherein counting

from commencement of the closing of the forming tool to complete forming, the

joint forming of the heated composite sheet structure introduced in a defined

position into the open forming tool takes place in 3 to 5 seconds.

Claim 7 (original): Method according to Claim 1, wherein cooling of the

jointly formed composite sheet structure takes place, at least in a first cooling

Page 3 of 14

U.S. Appln. Serial No. 09/972,195

Amendment Dated: June 2,6 2006

Reply to Office Action: February 27, 2006

phase on the forming tool, by contacting with the forming tool positively cooled

from inside.

Claim 8 (previously presented): Method according to Claim 7,

wherein the patched composite sheet structure remains in the forming tool

which is kept closed after the joint forming and is cooled down to at least to

about 500°C.

Claim 9 (original): Method according to Claim 1, wherein the patched

composite sheet structure remains in the forming tool which is kept closed after

the joint forming and is first cooled to about 500°C and is subsequently

transferred into an adjacent openable and closeable fixing tool which, in the

closed state, comes into contact with the formed composite sheet structure

received therein on both sides over the surface by a dimensionally accurate

impression and continues to fix the desired forming state of the composite sheet

structure mechanically, and

wherein, in the hot state which then prevails the formed composite

sheet structure is trimmed by a trimming tool integrated in the fixing tool and

continues to be cooled by the positively cooled impression of the fixing tool.

Claim 10 (previously presented): Method according to Claim 1,

wherein after the joint forming, the positive cooling of the patched composite

sheet structure is carried out first in the forming tool and subsequently, with

the desired forming state of the composite sheet structure constantly being

Page 4 of 14

fixed mechanically, by a sequence of adjacent openable and closeable fixing

tools which, in a closed state, come into contact on both sides over the surface,

with the composite sheet structure received in each case therein by a

dimensionally accurate impression, the composite sheet structure being passed

on from fixing tool to fixing tool and being cooled to at least 150°C in a plurality

of successive stages by impressions of the fixing tools, said impressions being

positively cooled from inside.

Claim 11 (previously presented): Method according to Claim 1,

wherein the patched composite sheet structure is cooled after the joint forming

either by the forming tool alone or jointly with a subsequent sequence of fixing

tools for 20-40 seconds.

Claim 12 (original): Method according to Claim 10, wherein the

patched composite sheet structure is cooled after the joint forming either by the

forming tool alone or jointly with a subsequent sequence of fixing tools for 20-

40 seconds, preferably about 25–30 seconds.

Claim 13 (original): Method according to Claim 1, wherein to achieve a

martensitic material structure in the formed composite sheet structure, the

latter is cooled at least in the temperature range between 800°C and 500°C,

rapidly, that is to say from 800°C to 500°C in less than four seconds.

Claim 14 (original): Method according to Claim 1, wherein the formed

composite sheet structure is cooled to achieve a bainitic material structure, at

U.S. Appln. Serial No. 09/972,195 Amendment Dated: June 2.6 2006

Reply to Office Action: February 27, 2006

least in the temperature range between 800°C and 500°C, comparatively slowly from 800°C to 500°C in a timespan lasting longer than four seconds.

Claim 15 (previously presented): Method for the production of a three-dimensionally shaped structural part having a basic sheet and at least one smaller locally arranged reinforcing sheet, comprising connecting the basic sheet, in a flat state or in an incompletely formed preforming state, to the reinforcing sheet at a point predetermined for a subsequent reinforcing point, and subsequently joint forming the parts of a resulting patched composite sheet structure by an openable and closeable forming tool in a forming press, wherein heating of the patched composite sheet structure before the joint forming to a temperature which is above a forming temperature of the material, then forming the patched composite sheet structure in a hot state into a desired shape with subsequently cooling thereof in the forming tool in a closed state, or in a following fixing tool, with a desired forming state being fixed mechanically, wherein, the reinforcing sheet is affixed to the basic sheet, at least one of the sheets is provided on its contact surface with a hard solder in a surface-covering manner, the latter being melted during heating to forming temperature and the jointly formed composite sheet structure being cooled at least up to the complete solidification of the hard solder, with the forming state being fixed mechanically in the forming tool which is kept closed.

Claim 16 (original): Method according to Claim 15, wherein the contact surface of the at least one sheet provided with hard solder is provided

with an excess of hard solder and this excess is expressed at an edge of the reinforcing sheet during the joint forming.

Claim 17 (original): Method according to Claim 15, wherein the contact surfaces both of the basic sheet and of the reinforcing sheet are cleaned and/or activated for hard soldering before the application of hard solder.

Claim 18 (original): Method according to Claim 15, wherein the hard solder is applied in paste form.

Claim 19 (original): Method according to Claim 15, wherein the hard solder is applied in the form of chips.

Claim 20 (original): Method according to Claim 15, wherein the hard solder is applied in the form of a soldering foil blank punched out according to shape.

Claim 21 (original): Method according to Claim 15, wherein a hard solder, the solidification temperature of which is at least 500°C, preferably at least 550°C, is used.

Claim 22 (original): Method according to Claim 15, wherein, after the application of the hard solder and after the reinforcing sheet has been laid in a defined position onto the basic sheet, the two are provisionally fixed to one another by a single tacking point.

Claim 23 (original): Method according to Claim 1, wherein the heating of the patched composite sheet structure takes place in a furnace in a protective-gas atmosphere.

Claim 24 (original): Method according to Claim 15, wherein the heating of the patched composite sheet structure takes place in a furnace in a protective-gas atmosphere.

Claim 25 (original): Method according to Claim 1, wherein the basic sheet and/or the reinforcing sheet consists of a water-hardening heat-treatable steel having the alloying composition listed below, where the contents are to be understood in % by weight and are to be added in addition to iron as the basic metal:

Carbon: 0.23 - 0.27%,

Silicon: 0.15 - 0.50%,

Manganese: 1.10 - 1.40%,

Chromium: 0.10 - 0.35%,

Molybdenum: 0 - 0.35%,

Titanium: 0.03 - 0.05%,

Aluminum: 0.02 - 0.06%,

Phosphorus: max. 0.025%,

Sulphur: max. 0.01%, and

Others in total: 0.0020 - 0.0035%.

Reply to Office Action: February 27, 2006

Claim 26 (original): Method according to Claim 15, wherein the basic sheet and/or the reinforcing sheet consists of a water-hardening heat-treatable steel having the alloying composition listed below, where the contents are to be understood in % by weight and are to be added in addition to iron as the basic metal:

Carbon:

0.23 - 0.27%

Silicon:

0.15 - 0.50%,

Manganese: 1.10 - 1.40%,

Chromium:

0.10 - 0.35%

Molybdenum:

0 - 0.35%

Titanium:

0.03 - 0.05%

Aluminum:

0.02 - 0.06%

Phosphorus: max. 0.025%,

Sulphur:

max. 0.01%, and

Others in total:

0.0020 - 0.0035%.

Claim 27 (original): Method according to Claim 1, wherein at least one of the basic sheet and the reinforcing sheet is precoated inorganically against corrosion and consists of a steel having the alloying composition listed below, where the contents are to be understood in % by weight and are to be added in addition to iron as the basic metal:

Carbon:

0.20 - 0.25%

U.S. Appln. Serial No. 09/972,195 Amendment Dated: June 2.6 2006 Reply to Office Action: February 27, 2006

Silicon:

0.15 - 0.35%,

Manganese: 1.10 - 1.35%,

Chromium:

0.10 - 0.35%,

Titanium:

0.02 - 0.05%

Sulphur:

max. 0.008%, and

Others in total:

0.002 - 0.004%.

Method according to Claim 1, wherein the Claim 28 (original): material strength of the composite sheet structure is increased to about 1300 - 1600 MPa by the heat treatment integrated into the process of joint hot forming.

Claim 29 (original): Method according to Claim 15, wherein the material strength of the composite sheet structure is increased to about 1300 - 1600 MPa by the heat treatment integrated into the process of joint hot forming.

Claim 30 (original): Method according to Claim 1, wherein locally reinforced shell parts for hollow members integrated into the passenger cell of a vehicle body are produced by means of this method.

Claim 31 (original): Method according to Claim 15, wherein locally reinforced shell parts for hollow members integrated into the passenger cell of a vehicle body are produced by means of this method.

Claim 32 (original): Method according to Claim 1, wherein locally reinforced shell parts for hollow members integrated into the chassis of a vehicle are produced by means of this method.

Claim 33 (original): Method according to Claim 15, wherein locally reinforced shell parts for hollow members integrated into the chassis of a vehicle are produced by means of this method.

Claims 34-48 (canceled).

Claim 49 (previously presented): Method according to Claim 1, wherein the patched composite sheet structure is cooled after the joint forming either by the forming tool alone or jointly with a subsequent sequence of fixing tools for about 25-30 seconds.

Claim 50 (new): Method according to claim 5, wherein the timespan is less than two seconds.